



Rapidly Tunable RF Cavity Development

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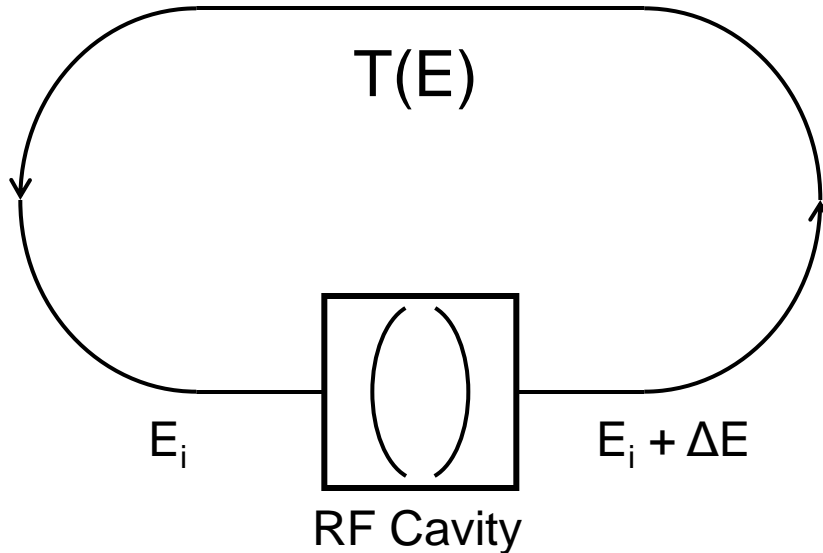
FAR-TECH, Inc.

- Located in San Diego, CA
- Founded in 1994, formerly known as **F**usion and **A**ccelerator **R**esearch (FAR), to pursue fusion and accelerator related research, technology and development.
- Core staff of over 10 PhDs Physics/Engineering
- Facility:
 - **Linux cluster** (88 processors) with 96GB of memory via Infiniband connection; 15 TB redundant storage
 - **RF, UHV, laboratory and assembly**

Motivation

- **Rapid-Cycling Accelerators (synchrotron, FFAG) have varying revolution times on successive orbits, requiring a different accelerating cavity frequency for each cycle.**
- **Ferromagnetic (ferrite) tuning cannot adjust the frequency of the cavity rapidly enough**
- **Low Q solutions (magnetic alloy or high external Q) waste RF power by dumping the energy after every revolution**
- **Ferroelectric (FE) material in accelerator applications have shown response times $< 10\text{ns}$**
- **FAR-TECH is developing a ferroelectric tuned cavity in the frequency range 325 – 350 MHz as a start**

The Problem in a Nutshell

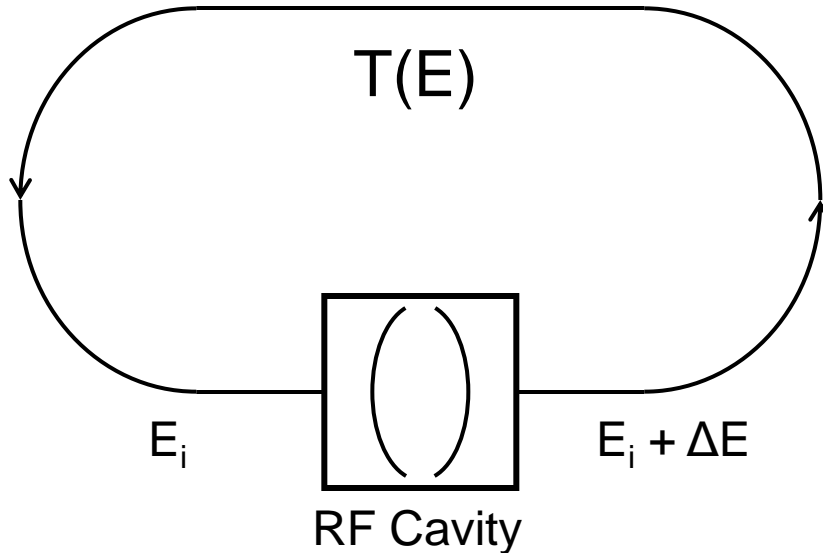


Cartoon Schematic of a Generic
Recirculating Accelerator
(from a cavity perspective)

- Want $\phi_{rf}/2\pi$ to be an integer for on-crest acceleration
- For fixed frequency, this only happens if f is a harmonic of $1/T$
- This makes fixed frequency acceleration difficult if T changes (which it does)

$$\frac{\phi_{rf}}{2\pi} = \int_{t_i}^{t_i+T} f(t) dt$$

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- This makes fixed frequency acceleration difficult if T changes (which it does)
- For **changing** frequency, adjust $f(t)$ such that the phase change between crossings ($\varphi_{rf}/2\pi$) is an integer
- The time history of the frequency is just as important as the size of the change in frequency over the revolution

$$\frac{\varphi_{rf}}{2\pi} = \int_{t_i}^{t_i+T} f(t) dt$$

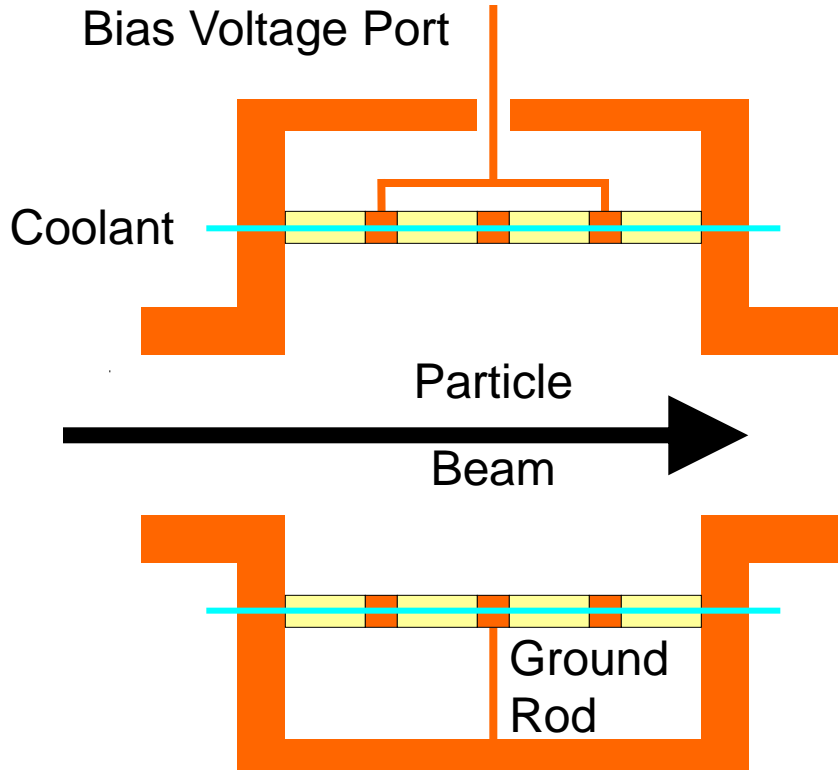
Low Q vs. “Higher” Q RF Cavity

- Low Q RF Cavity ($Q \sim 2-300$)
 - Wide resonance implies
 - ♦ Stored RF energy is “dumped” between cavity crossings
 - ♦ Greater RF losses
 - ♦ Generally does not require active tuning
 - Short fill time allows for replacement of RF power at the appropriate phase between cavity crossings
- “Higher” Q RF Cavity ($Q > 1000$)
 - Must be actively tuned
 - Narrow resonance implies lower RF losses
 - **Stored energy is “conditioned” and remains in the cavity for many cycles**
 - To maintain stable power levels, the RF power feed must be synchronous in both *frequency* and *phase* with the stored energy in the cavity

Ferroelectrics are the key

- Ferroelectric materials change permittivity (ϵ) when exposed to a biasing electric field and can have low loss tangent
 - ϵ changes with changing **electric field bias**
 - Low loss tangent does not mean low losses due to high ϵ
Loss $\propto \epsilon \tan\delta$
 - Material response time < 10 ns (limit of manufacturer's testing)
- Ferroelectric tuning is directly analogous with ferrite tuning
 - Permittivity change results in a frequency shift
 - Tuning strength is based on the fraction of electric RF field stored energy
 - Heat mitigation is a primary concern
- The effect of a large change in the dielectric constant results in non-linear perturbation of the RF field patterns

What Might a Cavity Look Like?

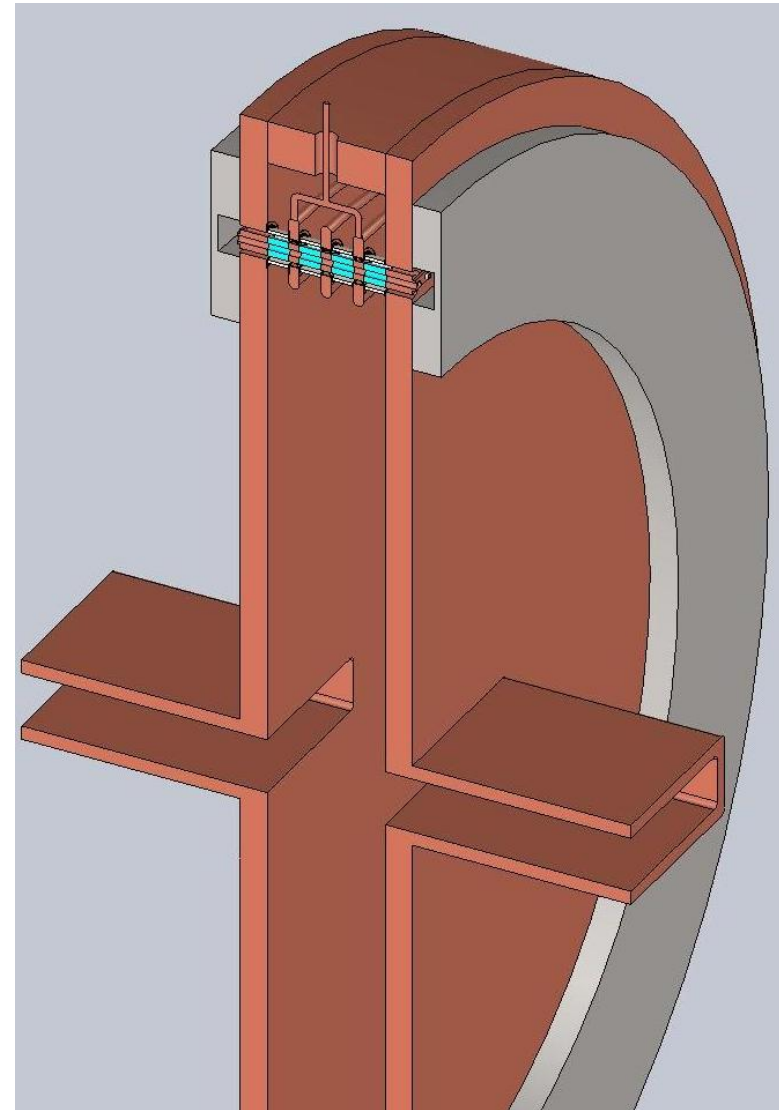


- Off-axis ferroelectric tubes separated by electrodes
- Reduces tuning effect compared to on-axis
- Reduces heat dissipation in ferroelectric
 - Dielectric constant is temperature dependent
- Tubes separate cavity vacuum from central portion of tube
 - Allows the use of dielectric coolant
 - Real design has ability to remove ferroelectric cartridge from cavity without vacuum break

A Semi-Conceptual Tunable Cavity Design

- For $\Delta f_{\text{full bias}} = 25 \text{ MHz}$, the estimated (realistic) phase shift is 2π in $1 \mu\text{s}$ (0.3π in 150 ns)

Property	Unbiased	Biased
Permittivity, ϵ	450	322
Frequency (MHz)	376	400
Q-Factor	3970	5890
Copper Losses (W)	3640	2070
Ferroelectric Losses (W)	4200	1510
Total Losses (W)	7840	3580
Energy Gain ($\beta = 0.4$) (keV)	30	30
RF Energy in Vacuum (mJ)	6.8	6.2
RF Energy in Ferroelectric (mJ)	6.3	2.1
ZTT (M Ω /m)	0.57	1.26
r/Q (Ω)	29.0	42.7



For an unloaded pillbox cavity (no beam pipe) of the same radius:

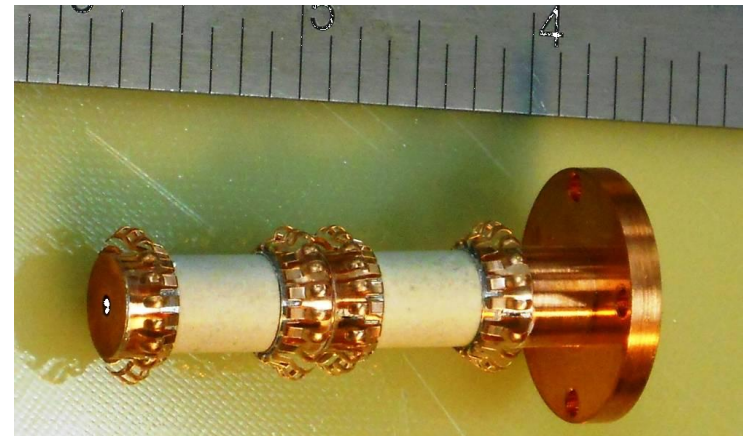
$$f = 428.9 \text{ MHz}$$

$$Q = 22800$$

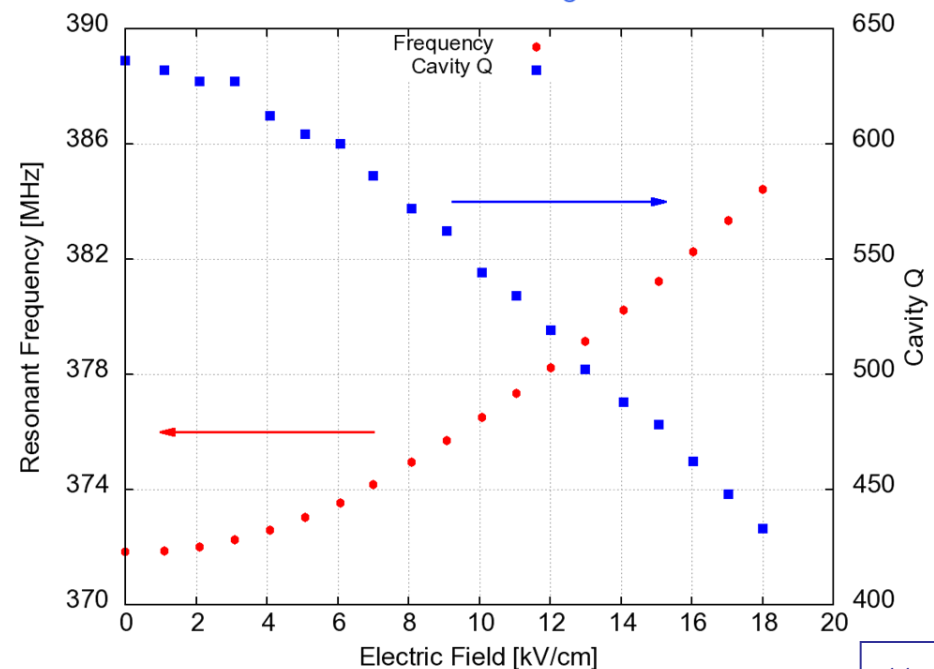
Cartridge Cold Test



- Cartridge on cavity axis to increase RF electric field
- Initially used to test construction details
- Used to prepare for High Power Equivalent (HPE) test cell experiments



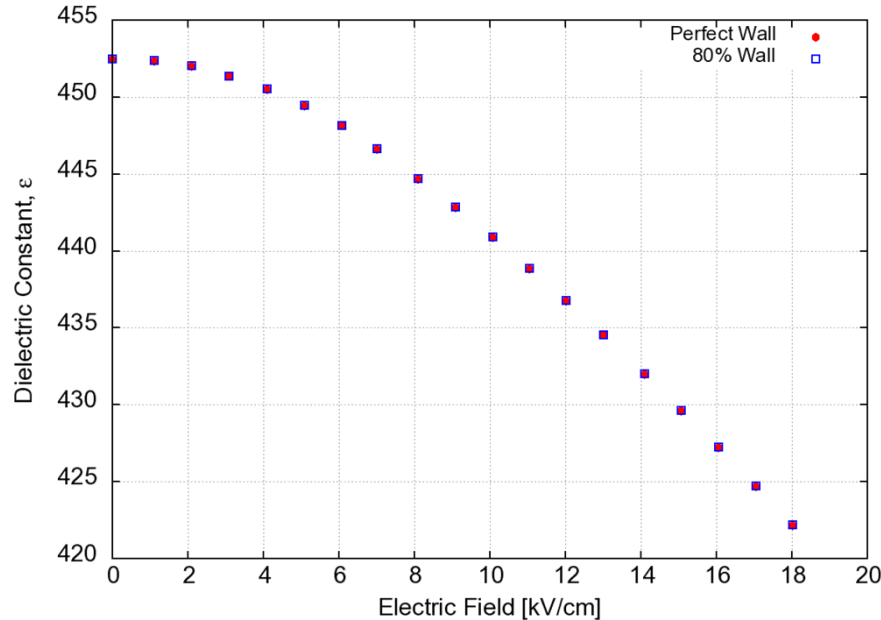
Measured Bias Cartridge Values



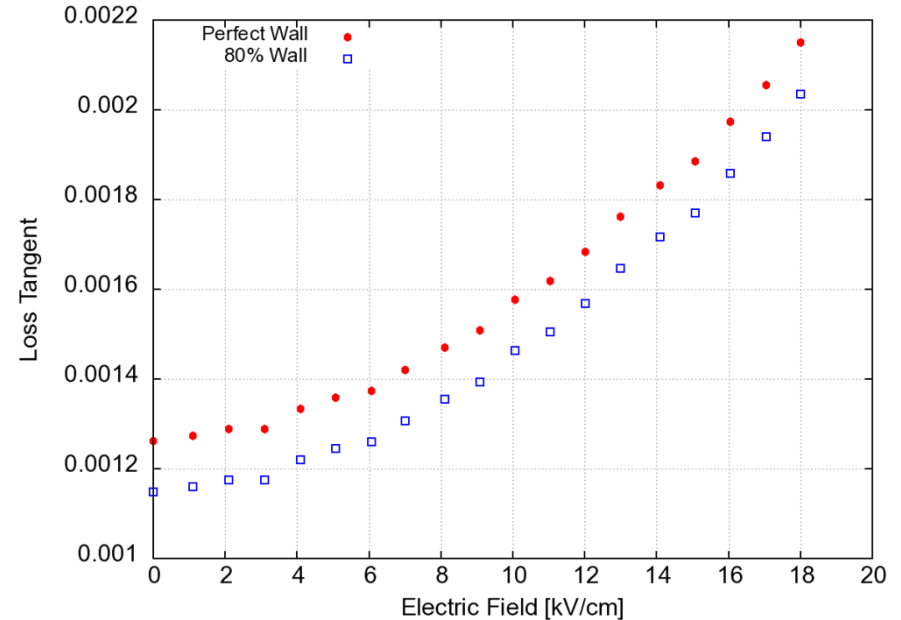
Ferroelectric material from Euclid Techlabs

ϵ and $\tan\delta$ from Cold Test Data

Dielectric Constant Based on Measured Data

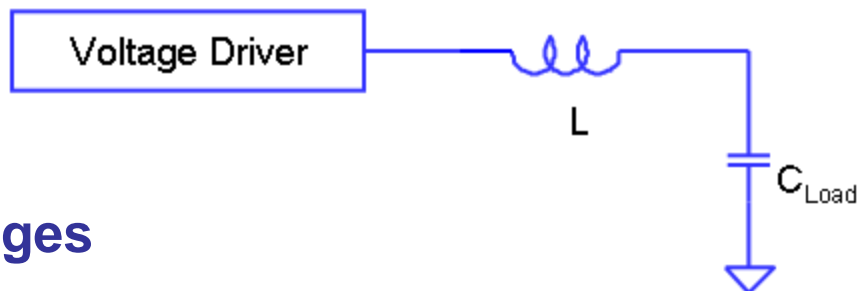
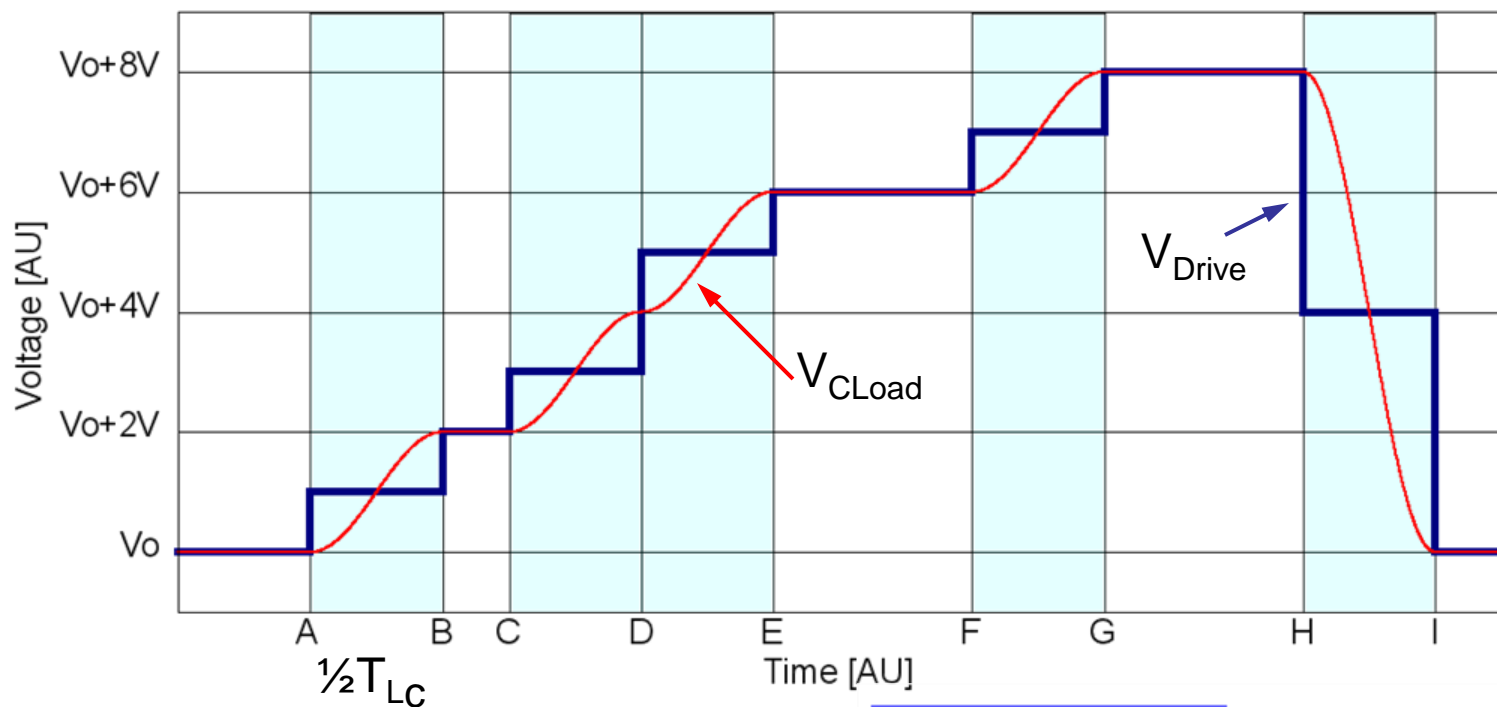


Loss Tangent Based on Measured Data



- FE losses from $\tan\delta$ only – termination effects folded into bulk losses
- HFSS simulations to determine (f, Q) from $(\epsilon, \tan\delta)$
- $Q = Q_{\text{wall}} \parallel Q_{\text{FE}}$
 - Reduction of Q_{wall} to 80% HFSS value to account for contact losses
- Use simulation data to determine $(\epsilon, \tan\delta)$ from measured (f, Q) – cubic spline interpolation

A Scenario of Voltage Ramp on C_{Load}



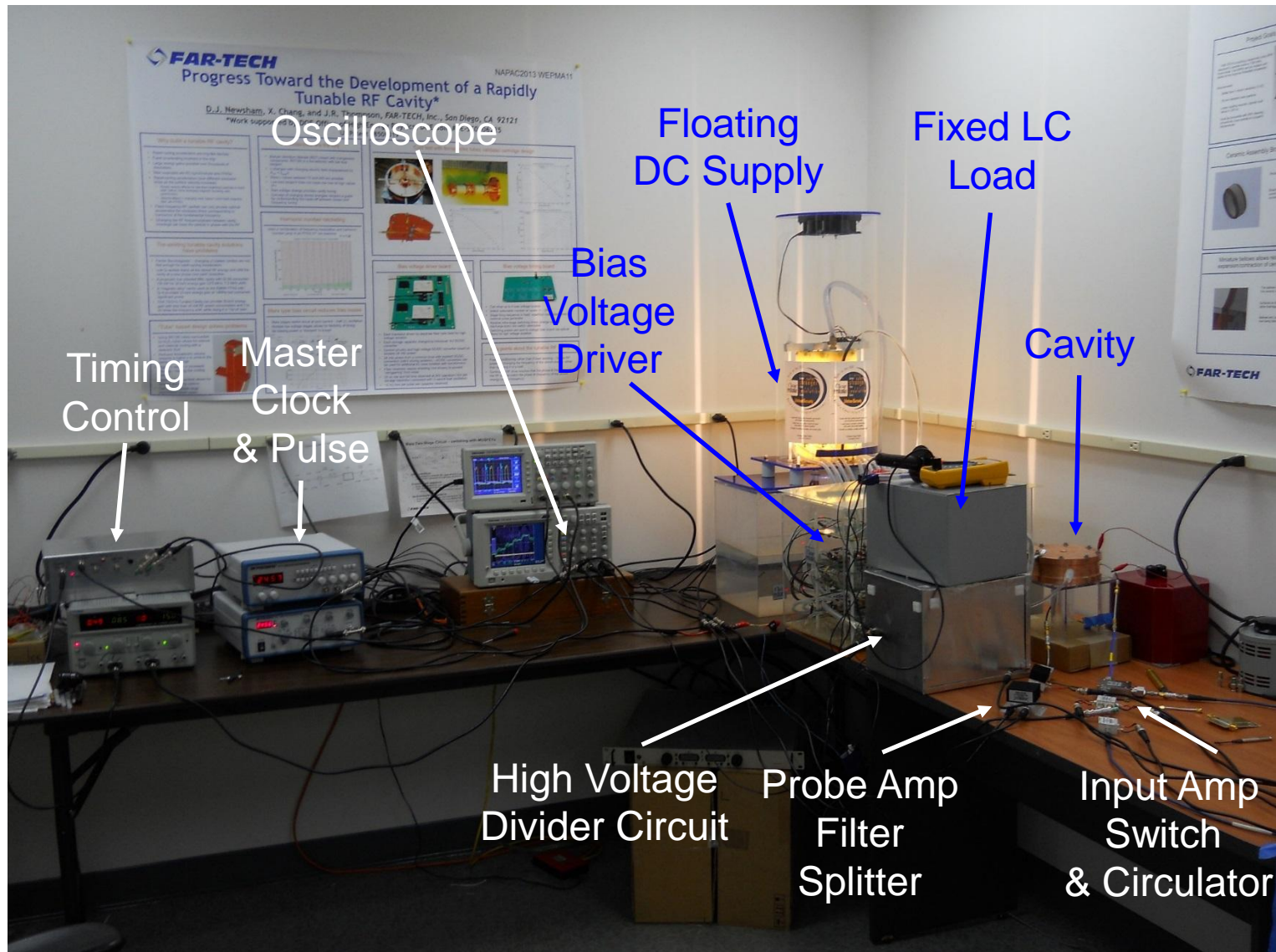
Ferroelectric cartridge is C_{Load}

Scenario with 4 bias voltage driver stages

Delay between (dis)charge and park (shaded) is $\frac{1}{2}T_{LC}$

Arbitrary delay between park and next (dis)charge

Voltage Driver Test on Cold Cavity

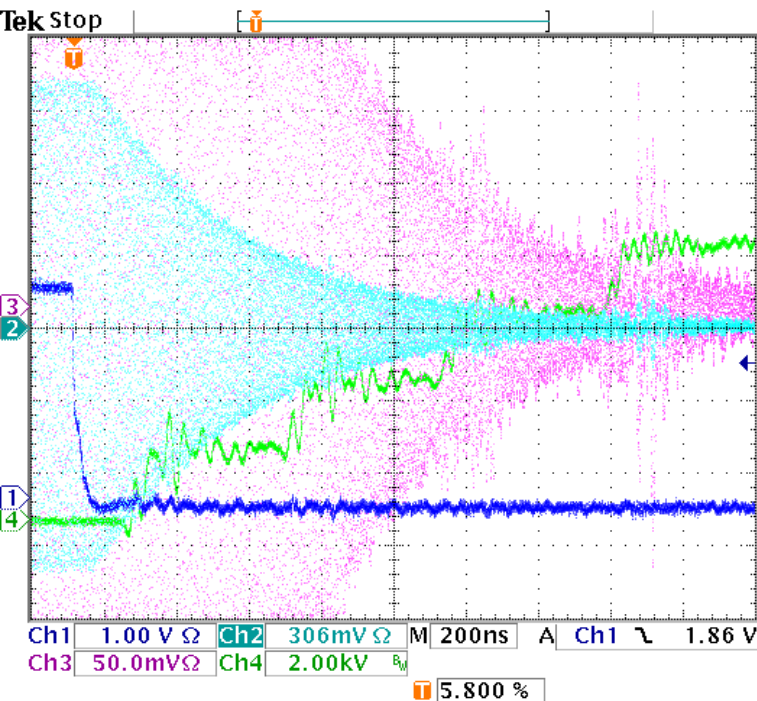


Frequency Shift Analysis – Initial Study

- Measure cavity field probe voltage with oscilloscope
 - Tektronix TDS 3054C 500MHz oscilloscope
 - 5 GS/sec – greater than 5x Nyquist
 - 10,000 sample record – allows 2 μ s window at full resolution
- **Numerical IQ Demodulation – Data Analysis Method**
 - Create numerical cosine and sine signal to serve as local oscillator for I and Q
 - Multiply each with measured data
 - Strong low pass filter to isolate difference frequency and remove noise
 - Determine phase, $\phi = \text{ArcTan}(\text{cosine}, \text{sine})$
 - ♦ Gives instantaneous phase of the RF signal relative to the local oscillator (with $-\pi$ to π wrapping)
 - Derivative of $\text{phase}/2\pi$ gives linear frequency shift

8kV Bias Test

HV pulse rate ~ 2.24 MHz
HV rise/fall ~ 85 ns

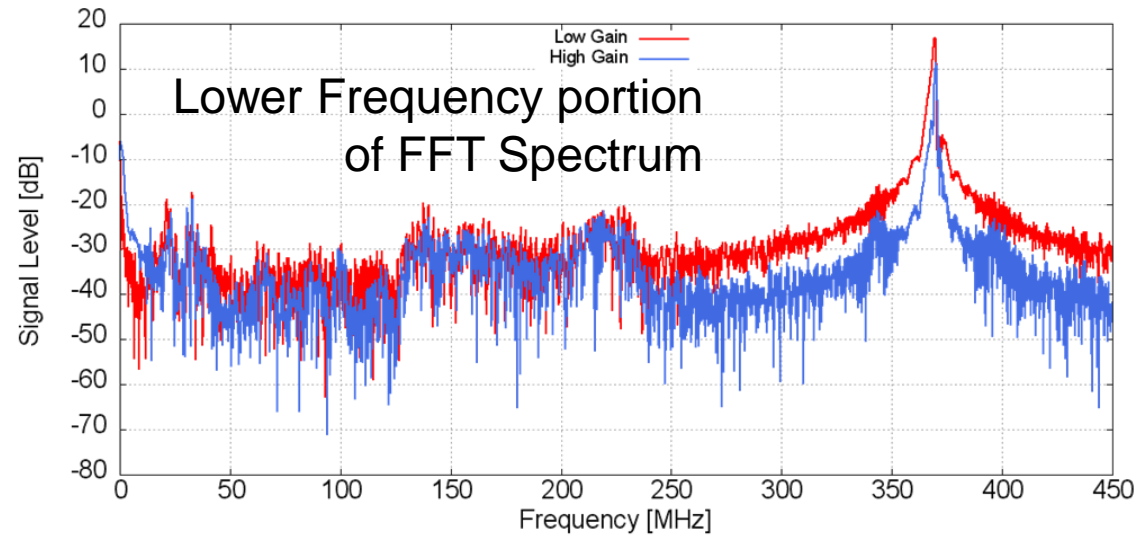


RF Switch (trigger)

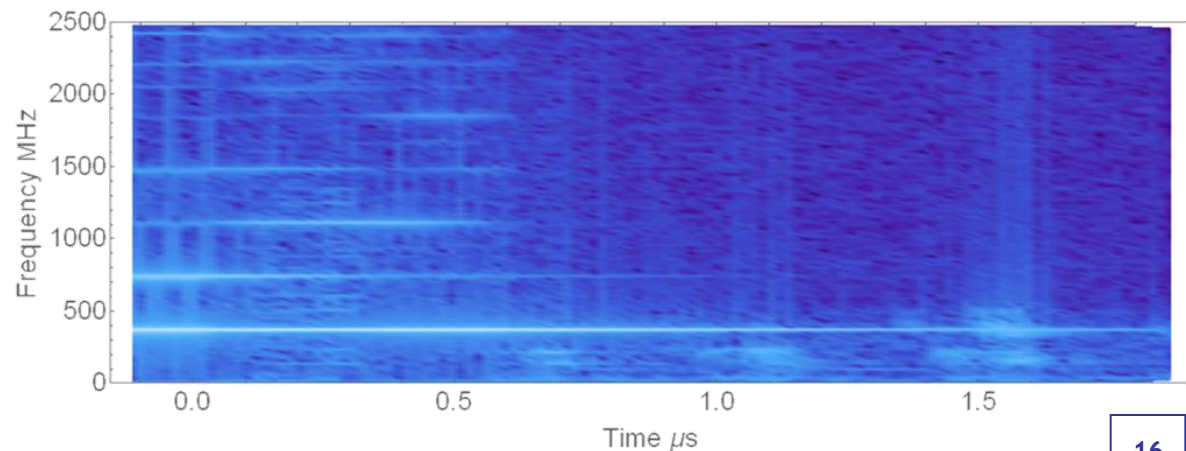
Low Gain

High Gain

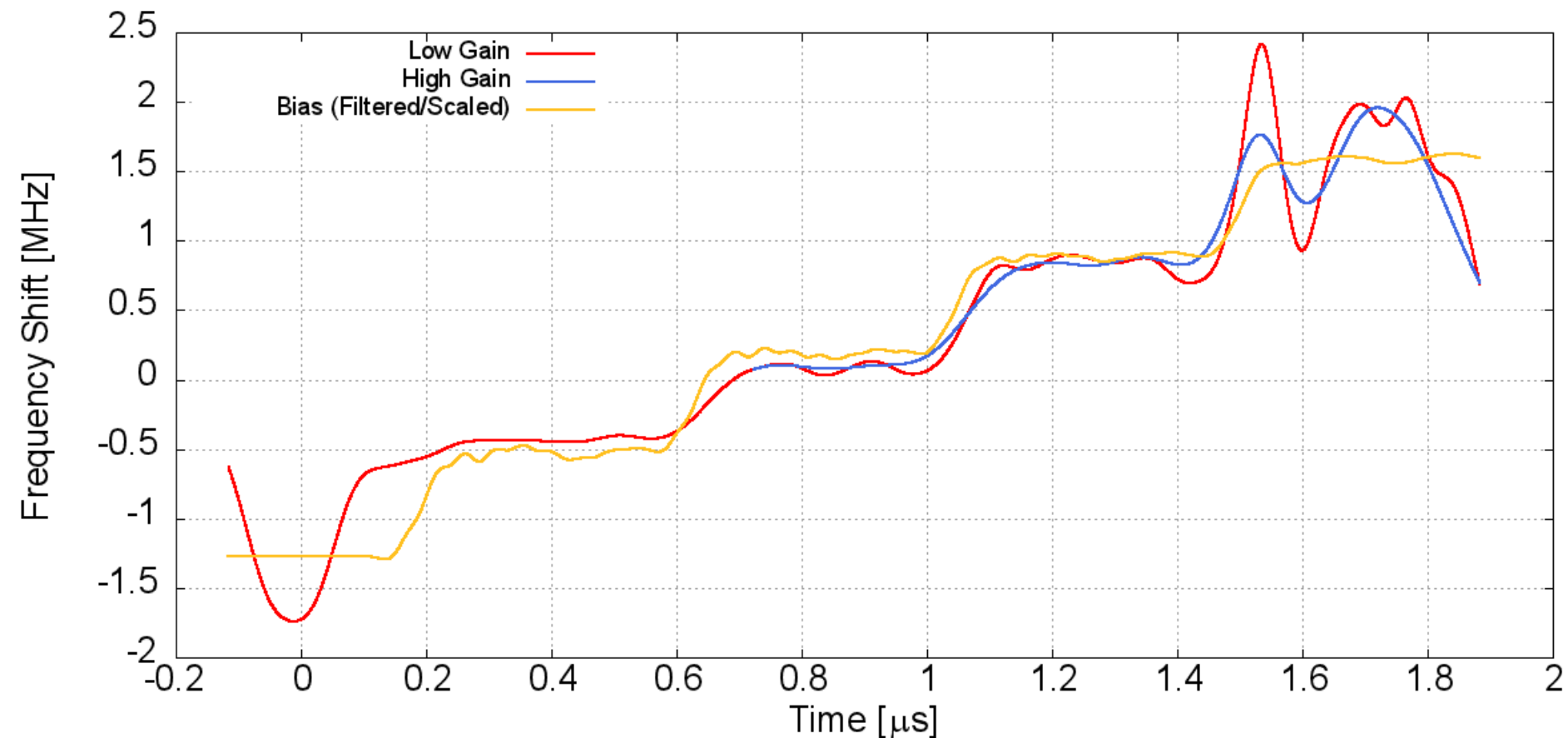
Voltage on C_{Load}



High Gain Spectrogram



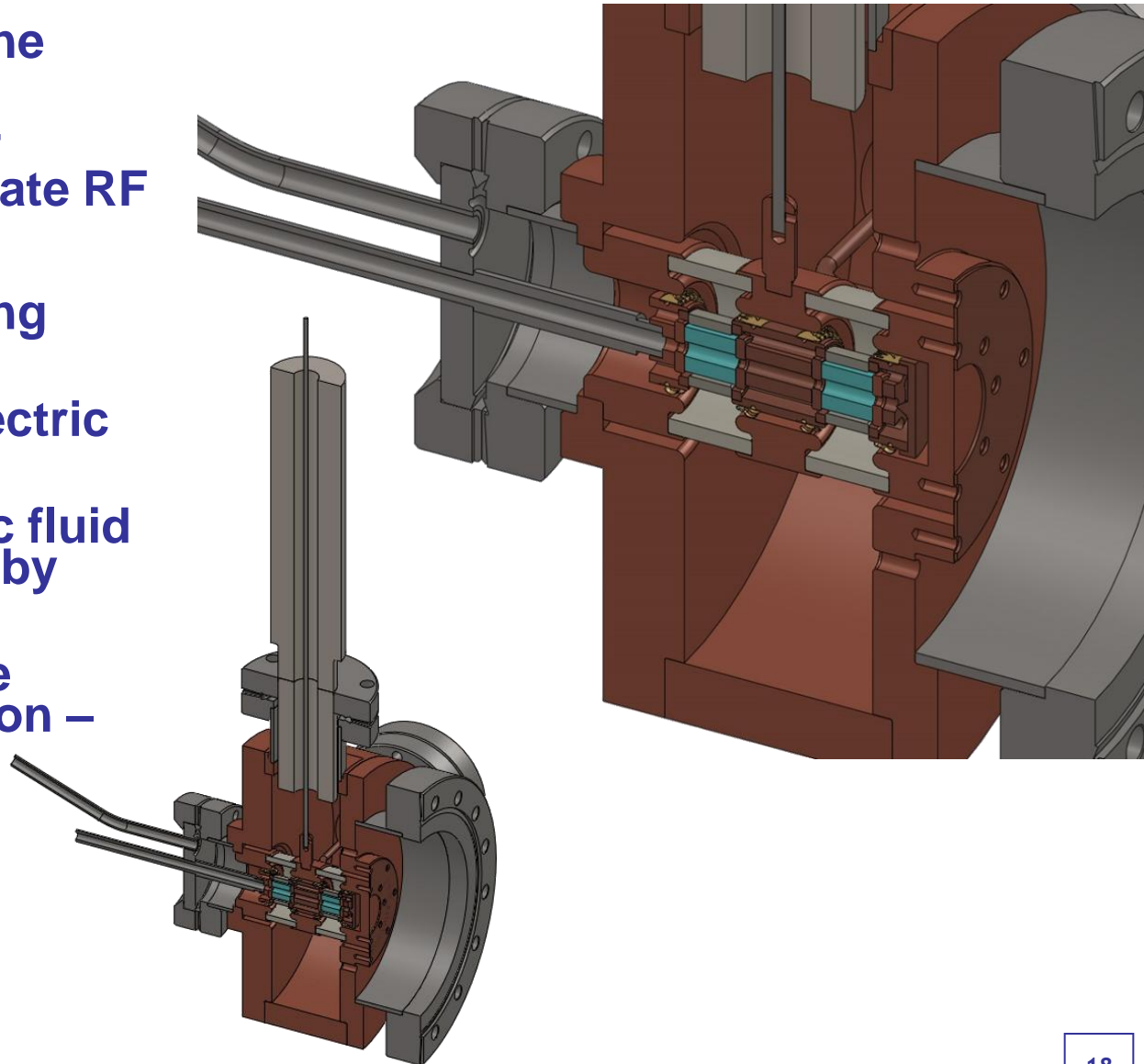
Frequency Shift – 8kV Bias Test



$F_{LO} = 370.0 \text{ MHz}$

High Power Equivalent Test Cell & Cartridge (under construction)

- The goal is to determine maximum possible RF electric field on the FE
- Purposefully concentrate RF electric field on FE to reduce RF power requirements by placing cartridge on axis
- FE is cooled with dielectric fluid in a series flow
- Vacuum, and dielectric fluid coolant are separated by outer layer of Al₂O₃
- Cartridge is removable under vacuum operation – **major advantage**



8kV Pulse Results Summary

- ~ **2.25 MHz** frequency shift in **1.4 μ s** presented with 8kV bias (**2.25 MHz** in **750 ns** observed)
- The frequency shift of a real cavity would be smaller because the test cell is purposefully enhanced (factor of 2-3)
- The switching noise contaminates all signals
 - Master clock
 - Timing control board
 - Bias voltage measurement
 - Oscilloscope itself
 - Input and output amplifier supply voltages
- Faraday cage impractical to implement given time and budget
- Analog high-pass filters for RF signals before digitizing creates some artifacts
- Continue tests on cold cavity to improve technique while high power cell is being constructed

END

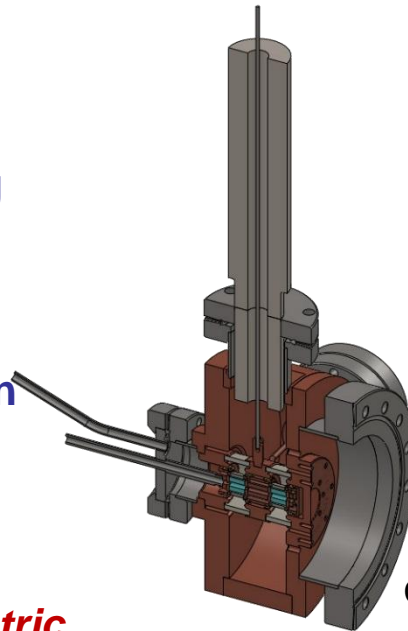
Tunable Cavity Development

Motivation

- Rapid-Cycling Accelerators (synchrotron, FFAG) require fast frequency tuning of the accelerating cavity
- Ferrite cavities are too slow, low Q cavities waste power
- Potential uses include proton/C⁶⁺ ion cancer therapy accelerators and possibly sub-critical reactors

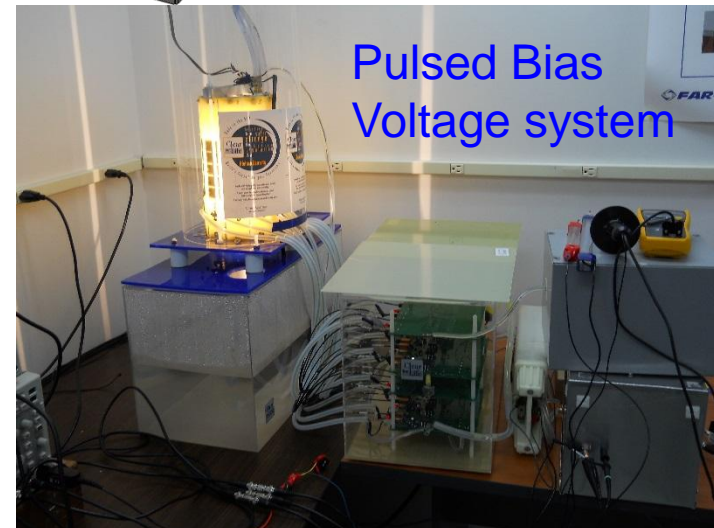
Development

- FAR-TECH is developing a ferroelectric tuned cavity in the frequency range 325 – 350 MHz as a start
- An actively cooled ferroelectric cartridge and high voltage bias generator are the top priorities
- ~ 2.5 MHz frequency shift at 8kV pulse bias with 2π phase shift in 750 ns was observed in cold testing



“Warm” Test Cavity for cartridge testing
UHV for voltage standoff
Active cooling with dielectric fluid
Cartridge can be removed under vacuum

Cartridge test cavity



Pulsed Bias Voltage system

Ferroelectric material from Euclid Techlabs